

MIC-SA-MAH 2174671

Hilti North America Installation Technical Manual Technical Data MI System

Version 1.2 08.2017





Terms of common cooperation / Legal disclaimer

The product technical data published in these Technical Data Sheets are only valid for the mentioned codes or technical data generation methods and the defined application conditions (e.g. ambient temperature load capacity not valid in case of fire, data not valid in support structures when mixed with third party products, values only apply to static loading conditions). Technical data applies to the component only — suitability and capacity of all other components must be checked separately by the responsible engineer (e.g., other assembly components, attachments, base materials, and building structures).

Suitability of structures combining different products for specific applications needs to be verified by conducting a system design and calculation, using for example Hilti PROFIS software. In addition, it is crucial to fully respect the Instructions for Use and to assure clean, unaltered and undamaged state of all products at any time in order to achieve optimum performance (e.g. avoid misuse, modification, overload, corrosion).

As products but also technical data generation methodologies evolve over time, technical data might change at any time without prior notice. We recommend to use the latest technical data sheets published by Hilti.

In any case the suitability of structures combining different products for specific applications need to be checked and cleared by an expert, particularly with regard to compliance with applicable norms, codes, and project specific requirements, prior to using them for any specific facility. This book only serves as an aid to interpret the capacity of the components listed, without any guarantee as to the absence of errors, the correctness and the relevance of the results or suitability for a specific application. User must take all necessary and reasonable steps to prevent or limit damage. The suitability of structures combining different products for specific applications need to be confirmed with a professional designer and/or structural engineers to ensure compliance with User's specific jurisdiction and project requirements.



Designation Item number MIC-SA-MAH 2174671

Corrosion protection:

Hot dipped galvanized per DIN EN ISO 1461:

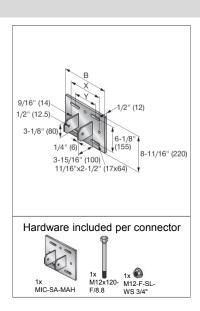
Connector: 2.2 mils (55 µm) Bolt: 1.8 mils (45 µm) Nut: 1.8 mils (45 µm)

Weight:

14.77 lb (6701g) incl. components

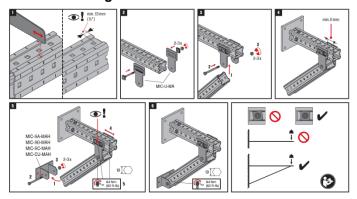
Description:

Hilti Hot-dipped galvanized baseplate connector, used for anchoring a MI-90 girder to a steel beam at an angle, usually when it's used as a brace for another girder. Four oblong anchor holes enable fine tuning of baseplate position, and girder is connected using one bolt through a hole, which enables various angles. For use with M16 hardware.

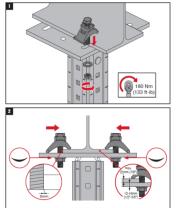


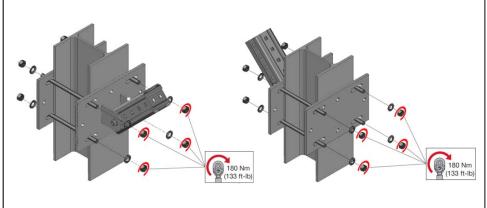
Material properties:				
Material	Yield strength	Ultimate strength	E-modulus	Shear modulus
Connector				
S235JR - DIN EN10025-2 2005.4	$f_y = 34.08 \text{ ksi } (235 \frac{N}{mm^2})$	$f_u = 52.21 \text{ ksi } (360 \frac{N}{mm^2})$	E = 29000 ksi (200000 $\frac{N}{mn}$	$(\frac{N}{m^2})$ G = 11000 ksi $(75845 \frac{N}{mm^2})$
Hexagonal head screw, prevail torque	hex nut	nene	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	nene
Class 8.8 - DIN EN 1993-1-8	$f_y = 92.82 \text{ ksi } (640 \frac{N}{mm^2})$	$f_u = 116.03 \text{ ksi } (800 \frac{N}{mm^2})$) E = 29000 ksi (200000 $\frac{N}{mn}$	$(\frac{1}{m^2})$ G = 11000 ksi $(75845 \frac{N}{mm^2})$

Instruction For Use: For both loading cases:

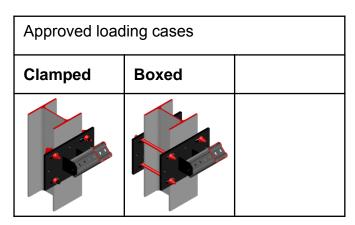


For clamped loading case For boxed loading case (not attached to the packaging)









Governing Conditions

Methodology:

Connection strength values are determined with a combination of simulation (ANSYS®), calculation (Microsoft Excel and Mathcad) and testing.

Standards and codes:

ANSI/AISC 360-10 Specification for Structural Steel Buildings

ANSI/AISC 360-10-Inelastic analysis

Appendix 1

AISC Steel Design Column Base Plates

Guide Series 1

AISI S100 - 2007/2010 North American Specification for the Design of cold

formed Steel Structural Members

EN 1993-1-1 Eurocode 3: Design of steel structures – Part 1-1: 03.2012

General rules and rules for buildings

EN 1993-1-8 Eurocode 3: Design of steel structures – Part 1-8: 03.2012

Design of joints

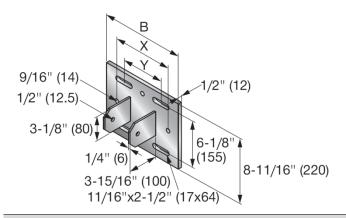
Hot rolled products of structural steels-Part 2: technical EN 10025-2 02.2005

delivery conditions for non-alloy structural steels

Validity:

Temperature limits: -22°F (-30°C) to 200°F (+93°C).

Published allowable loads for applications are based on static loading conditions. Non-static forces, including those resulting from thermal or other expansion must be taken into account during design.





Clamped	Boxed	
The loop Steep and Houlek Steep talks on the bloom, pages to the steep station better		
1 Marie de propri la prili prinde		
1 Propieto in protest senio (- filoso IIII/8)		
falmel at a region in plu to per firedo aplane falmel at an the appsolo pite are falmel at a as talk a P _e and		

Loading case: Clam	ped	Combinations covered by loading case
Bill of Material for the MIC-SA-MAH Hardware not include Beam clamps 4x MI-SGC M16	2174671	Connector used for an angled connection of MI-90 to structural steel profiles (bracing). For flange width 2.95" (75mm) -6.47" (165mm).

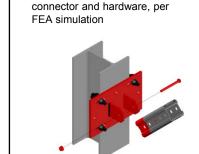
Usage of Values for Design Strength and Allowable Strength

The Design Strength and Allowable Strength tables on the following pages include strength reduction factors:

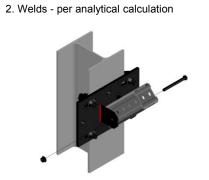
- ASD: Safety Factor (omega) > 1.0 as per AISC specifications.
- **LRFD:** Strength Reduction Factor (phi) < 1.0 as per AISC specifications. $\Omega = \frac{1.5}{b}$ (Reference AISC 360 C-B3-5)

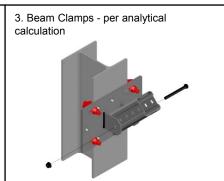
Factored loads are required for input to the given interaction equations. Factored loads are the responsibility of the user. Factored loads are noted as P, V and M

Limiting components of capacity evaluated in following tables:



1. Connection system, including





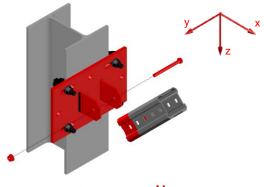


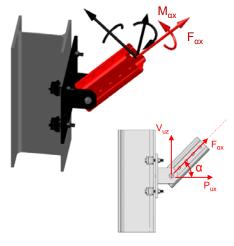
Clamped	Boxed	

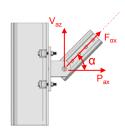
Values for Design Strength and Allowable Strength

NOTE: Calculate interaction separately for each group only using values from that group. Limiter is defined by highest interaction. Use absolute values. Values refer to the coordinate system shown.

1. Connection system, including connector and hardware, per FEA simulation







		+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
	LRFD*	3.75	3.75	1.48	1.48	3.75	3.75
	LINID	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
		0.52	0.52	0.00	0.00	0.00	0.00
1							
		+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
	4 CD*			,	,	. –	
	ASD*	[kip]	[kip]	[kip]	[kip]	[kip]	[kip]

Note: Design Strength values for girder Torsion about the αx -axis ($M_{\alpha x}$) are valid for any bracing angle.

Values include verification of hexagonal bolt

Interaction for LRFD

Due to the fact, that the same resistance values as for MIC-CU-MA are decisive, the same

$$\left[\frac{P_{ux}}{F_x}\right]^2 + \left[\frac{V_{uz}}{F_z}\right]^2 + \frac{V_{uy}}{F_y} + \frac{M_{ux}}{M_x} \le 1$$

Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

 $P_{ux} = F_{\alpha x} \times \cos(\alpha)$ $Vuz = F_{\alpha x} x \sin(\alpha)$

Interaction for ASD:

$$\left[\frac{P_{ax}}{F_x}\right]^2 + \left[\frac{V_{az}}{F_z}\right]^2 + \frac{V_{ay}}{F_y} + \frac{M_{ax}}{M_x} \le 1$$

Use of F_{α} : In case only the force along the brace axis (αx) is known, determinate load components as follows:

$$P_{ax} = F_{\alpha x} \times \cos(\alpha)$$

 $Vaz = F_{\alpha x} \times \sin(\alpha)$

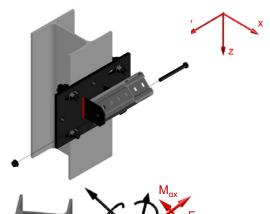


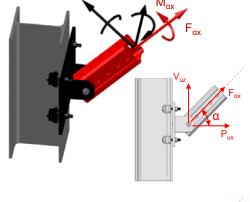
Clamped	Boxed	

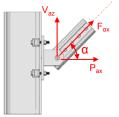
Values for Design Strength and Allowable Strength

NOTE: Calculate interaction separately for each group only using values from that group. Limiter is defined by highest interaction. Use absolute values. Values refer to the coordinate system shown.

2. Welds - per analytical calculation







[kip] 66.29	[kip]	[kip]	[kip]	[kip]	Flation 1
66 29			[P]	[KiP]	[kip]
	66.29	3.02	3.02	11.74	11.74
+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
1.87	1.87	0.00	0.00	0.00	0.00
+Fx	-Fx	+Fy	-Fy	+Fz	-Fz
[kip]	[kip]	[kip]	[kip]	[kip]	[kip]
44.19	44.19	2.01	2.01	7.83	7.83
+Mx	-Mx	+My	-My	+Mz	-Mz
kip*ft]	[kip*ft]	[kip*ft]	[kip*ft]	[kip*ft]	[kip*ft]
1.25	1.25	0.00	0.00	0.00	0.00
	+Fx [kip] 44.19 +Mx kip*ft] 1.25	kip*ft] [kip*ft] 1.87	kip*ft] [kip*ft] [kip*ft] 1.87 1.87 0.00 +Fx -Fx +Fy [kip] [kip] [kip] 44.19 44.19 2.01 +Mx -Mx +My kip*ft] [kip*ft] [kip*ft] 1.25 1.25 0.00	kip*ft] [kip*ft] [kip*ft] [kip*ft] [kip*ft] 1.87 1.87 0.00 0.00 +Fx -Fx +Fy -Fy [kip] [kip] [kip] [kip] 44.19 44.19 2.01 2.01 +Mx -Mx +My -My kip*ft] [kip*ft] [kip*ft] [kip*ft] 1.25 1.25 0.00 0.00	kip*ft] [kip*ft] [kip] [kip*ft] [kip*ft]

Note: Design Strength values for girder Torsion about the x-axis ($M_{\alpha x}$) are valid for any bracing angle.

$$\frac{P_{ux}}{F_x} + \frac{V_{uz}}{F_z} + \frac{V_{uy}}{F_y} + \frac{M_{ux}}{M_x} \le 1$$

Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

 $P_{ux} = F_{\alpha x} \times \cos(\alpha)$ $Vuz = F_{\alpha x} x \sin(\alpha)$

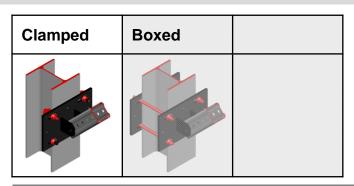
Interaction for ASD:

$$\frac{P_{ax}}{F_x} + \frac{V_{az}}{F_z} + \frac{V_{ay}}{F_y} + \frac{M_{ax}}{M_x} \le 1$$

Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

 $P_{ax} = F_{\alpha x} \times \cos(\alpha)$ $Vaz = F_{\alpha x} \times \sin(\alpha)$



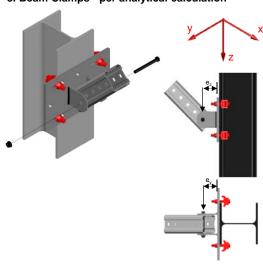


Values for Design Strength and Allowable Strength

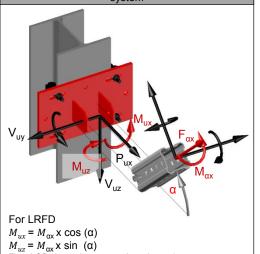
3/3

NOTE: Calculate interaction separately for each group only using values from that group. Limiter is defined by highest interaction. Use absolute values. Values refer to the coordinate system shown.

3. Beam Clamps - per analytical calculation



Transition of the forces generated on inclined
brace to base material connector's coordinate
system



For ASD (not shown on the picture)

 $M_{ax} = M_{ax} \times \cos(\alpha)$

 $M_{az}^{ax} = M_{\alpha x}^{\alpha x} x \sin (\alpha)$

	+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
LRFD*	21.57	Not decisive	2.32	2.32	2.32	2.32
LIVI D	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
	0.62	0.62	4.60	4.60	2.30	2.30
	+Fx	-Fx	+Fy	-Fy	+Fz	-Fz
	+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
∆SD*			,	,	. –	
ASD*	[kip]	[kip] Not	[kip]	[kip]	[kip]	[kip]

Interaction for LRFD

Normal force interaction:

The eccentricity ey and ez between the point of force transfer channel / connector and baseplate, which generates an additional bending moment on the system , must be taken into account in the interaction formula.

$$\frac{P_{ux}}{F_x} + \frac{V_{uy} \times ey}{M_z} + \frac{V_{uz} \times ez}{M_y} + \frac{M_{uz}}{M_z} \le 1$$

with $e_v = e_z = 0.070 \text{ m}$

Shear force interaction:

- Shear Interaction Equation is only valid for TENSILE P_{ux} loads (P_{ux} > 0). Equation is not valid for compressive P_{ux} loads (P_{ux} < 0).
 - For Shear interaction, user must ADDITIONALLY verify: $P_{ux} / F_x < 1$.

$$\left| \left(\frac{V_{uy}}{F_y \times \left(1 - \frac{P_{ux}}{F_x} \right)} \right)^2 + \left(\frac{V_{uz}}{F_z \times \left(1 - \frac{P_{ux}}{F_x} \right)} \right)^2 + \frac{M_{ux}}{M_x \times \left(1 - \frac{P_{ux}}{F_x} \right)} \le 1 \right|$$

Note: Due to the fact, that depending on the inclination of the channel, the acting torsional moment Max can either generate shear or tension, it will be considered in both interactions.

Interaction for ASD:

Normal force interaction:

The eccentricity ey and ez between the point of force transfer channel / connector and baseplate, which generates an additional bending moment on the system, must be taken into account in the interaction formula.

$$\frac{P_{ax}}{F_x} + \frac{V_{ay} \times ey}{M_z} + \frac{V_{az} \times ez}{M_y} + \frac{M_{az}}{M_z} \le 1$$

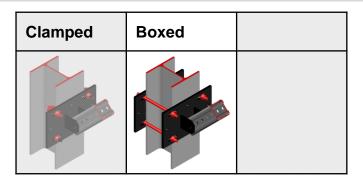
with e_y = e_z =0.070 m

Shear force interaction:

- Shear Interaction Equation is <u>only</u> valid for TENSILE P_{ax} loads ($P_{ax} > 0$). Equation is <u>not</u> valid for compressive P_{ax} loads ($P_{ax} < 0$).
- For Shear interaction, user must ADDITIONALLY verify: $P_{ax}/F_x < 1$.

$$\sqrt{\left(\frac{V_{ay}}{F_y \times \left(1 - \frac{P_{ax}}{F_x}\right)}\right)^2 + \left(\frac{V_{az}}{F_z \times \left(1 - \frac{P_{ax}}{F_x}\right)}\right)^2 + \frac{M_{ax}}{M_x \times \left(1 - \frac{P_{ax}}{F_x}\right)} \le 1}$$





Loading case: Boxed

Combinations covered by loading case

Bill of Material for this loading case:

1x MIC-SA-MAH 2174671

Hardware not included in packaging:

Base plate

1x MIB-SAH 2174674

Threaded rods cut to particular length 4x AM16x1000 8.8 HDG...m 419104

Lock washer

8x LW M16 HDG plus washer 2185343

Nut

8x M16-F nut 304767

Connector used for an angled connection of MI-90 to structural steel profiles (bracing). For flange width

2.95" (75mm) - 6.47" (165mm).



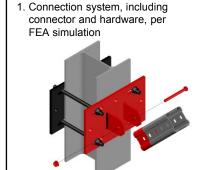
Usage of Values for Design Strength and Allowable Strength

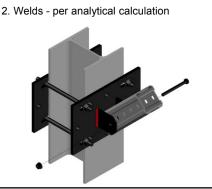
The Design Strength and Allowable Strength tables on the following pages include strength reduction factors:

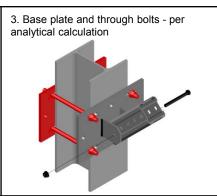
- 1. ASD: Safety Factor (omega) > 1.0 as per AISC specifications.
- 2. <u>LRFD:</u> Strength Reduction Factor (phi) < 1.0 as per AISC specifications. $\Omega = \frac{1.5}{\phi}$ (Reference AISC 360 C-B3-5)

Factored loads are required for input to the given interaction equations. Factored loads are the responsibility of the user. Factored loads are noted as P, V and M

Limiting components of capacity evaluated in following tables:







Installation Technical Manual - Technical Data - MI system

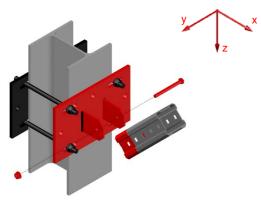


Clamped	Boxed	

Values for Design Strength and Allowable Strength

NOTE: Calculate interaction separately for each group only using values from that group. Limiter is defined by highest interaction. Use absolute values. Values refer to the coordinate system shown.

1. Connection system, including connector and hardware, per FEA simulation



	+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
LRFD*	3.75	3.75	1.48	1.48	3.75	3.75
LKFD	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
	0.52	0.52	0.00	0.00	0.00	0.00
	+Fx	-Fx	+Fy	-Fy	+Fz	-Fz
	[kip]	[kip]	[kip]	[kip]	[kip]	[kip]
Λ C D *	2.50	2.50	0.99	0.99	2.50	2.50
ASD*		N 4	1 N A	N 4	. N.A.	N 4
	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]

Note: Design Strength values for girder Torsion about the x-axis $(M_{\alpha x})$ are valid for any bracing angle.

Values include verification of hexagonal bolt

Interaction for LRFD

Due to the fact, that the same resistance values as for MIC-CU-MA are decisive, the same interaction formulation can be used:

$$\left[\frac{P_{ux}}{F_x}\right]^2 + \left[\frac{V_{uz}}{F_z}\right]^2 + \frac{V_{uv}}{F_y} + \frac{M_{ux}}{M_x} \le 1$$

Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

$$P_{ux} = F_{\alpha x} \times \cos(\alpha)$$

 $Vuz = F_{\alpha x} \times \sin(\alpha)$

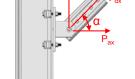
Interaction for ASD:

$$\left[\frac{P_{ax}}{F_x}\right]^2 + \left[\frac{V_{az}}{F_z}\right]^2 + \frac{V_{ay}}{F_y} + \frac{M_{ax}}{M_x} \le 1$$

Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

$$P_{ax} = F_{\alpha x} \times \cos(\alpha)$$

 $Vaz = F_{\alpha x} x \sin(\alpha)$



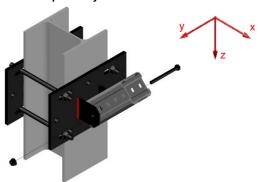


Clamped	Boxed	

Values for Design Strength and Allowable Strength

NOTE: Calculate interaction separately for each group only using values from that group. Limiter is defined by highest interaction. Use absolute values. Values refer to the coordinate system shown.

2. Welds - per analytical calculation



	+Fx	-Fx	+Fy	-Fy	+Fz	-Fz
LRFD*	[kip]	[kip]	[kip]	[kip]	[kip]	[kip]
	66.29	66.29	3.02	3.02	11.74	11.74
	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
	1.87	1.87	0.00	0.00	0.00	0.00
	+Fx	-Fx	+Fy	-Fy	+Fz	-Fz
ASD*	[kip]	[kip]	[kip]	[kip]	[kip]	[kip]
	44.19	44.19	2.01	2.01	7.83	7.83
	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
	1.25	1.25	0.00	0.00	0.00	0.00

Interaction for LRFD

Note: Design Strength values for girder Torsion about the x-axis $(M_{\alpha x})$ are valid for any bracing angle.

$$\frac{P_{ux}}{F_x} + \frac{V_{uz}}{F_z} + \frac{V_{uy}}{F_y} + \frac{M_{ux}}{M_x} \le 1$$

Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

$$P_{ux} = F_{\alpha x} \times \cos(\alpha)$$

 $Vuz = F_{\alpha x} \times \sin(\alpha)$

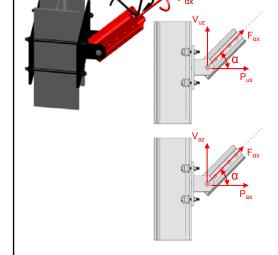
Interaction for ASD:

$$\frac{P_{ax}}{F_x} + \frac{V_{az}}{F_z} + \frac{V_{ay}}{F_y} + \frac{M_{ax}}{M_x} \le 1$$

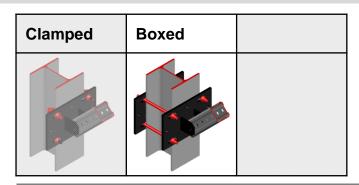
Use of $F_{\alpha x}$: In case only the force along the brace axis (αx) is known, determinate load components as follows:

$$P_x = F_{\alpha x} \times \cos(\alpha)$$

 $V_z = F_{\alpha x} \times \sin(\alpha)$



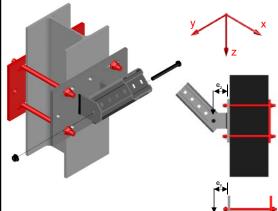


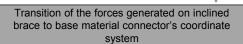


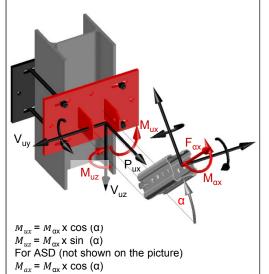
Values for Design Strength and Allowable Strength

NOTE: Calculate interaction separately for each group only using values from that group. Limiter is defined by highest interaction. Use absolute values. Values refer to the coordinate system shown.









 $M_{az} = M_{\alpha x} \times \sin (\alpha)$

LRFD*	+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
	34.58	Not decisive	7.26	7.26	7.26	7.26
	+Mx [kip*ft]	-Mx [kip*ft]	+My [kip*ft]	-My [kip*ft]	+Mz [kip*ft]	-Mz [kip*ft]
	1.93	1.93	6.81	6.81	4.54	4.54
			_			
	+Fx	-Fx	+Fy	-Fy	+Fz	-Fz
	+Fx [kip]	-Fx [kip]	+Fy [kip]	-Fy [kip]	+Fz [kip]	-Fz [kip]
ASD*					. –	
ASD*	[kip]	[kip] Not	[kip]	[kip]	[kip]	[kip]

Interaction for LRFD

Normal force interaction:

The eccentricity ey and ez between the point of force transfer channel / connector and baseplate, which generates an additional bending moment on the system, must be taken into account in the interaction formula.

$$\frac{P_{ux}}{F_x} + \frac{V_{uy} \times ey}{M_z} + \frac{V_{uz} \times ez}{M_y} + \frac{M_{uz}}{M_z} \le 1$$

Shear force interaction:

- Shear Interaction Equation is only valid for TENSILE P_{ux} loads ($P_{ux} > 0$). Equation is not valid for compressive P_{ux} loads ($P_{ux} < 0$). For Shear interaction, user must ADDITIONALLY verify: $P_{ux} / F_x < 1$.

$$\left| \left(\frac{V_{uy}}{F_y \times \left(1 - \frac{P_{ux}}{F_x} \right)} \right)^2 + \left(\frac{V_{uz}}{F_z \times \left(1 - \frac{P_{ux}}{F_x} \right)} \right)^2 + \frac{M_{ux}}{M_x \times \left(1 - \frac{P_{ux}}{F_x} \right)} \le 1 \right|$$

Note: Due to the fact, that depending on the inclination of the channel, he acting torsional moment $M\alpha x$ can either generate shear or tension, it will be considered in both interactions

Interaction for ASD:

Normal force interaction:

The eccentricity ey and ez between the point of force transfer channel / connector and baseplate, which generates an additional bending moment on the system, must be taken into account in the interaction formula.

interaction formula.
$$\frac{P_{ax}}{F_x} + \frac{V_{ay} \times ey}{M_z} + \frac{V_{az} \times ez}{M_y} + \frac{M_{az}}{M_z} \le 1$$

with $e_v = e_z = 0.070 \text{ m}$

Shear force interaction:

- Shear Interaction Equation is <u>only</u> valid for TENSILE P_{ax} loads ($P_{ax} > 0$). Equation is <u>not</u> valid for compressive P_{ax} loads ($P_{ax} < 0$).

 For Shear interaction, user must ADDITIONALLY verify: $P_{ax} / P_x < 1$.

$$\left| \left(\frac{V_{ay}}{F_y \times \left(1 - \frac{P_{ax}}{F_x} \right)} \right)^2 + \left(\frac{V_{az}}{F_z \times \left(1 - \frac{P_{ax}}{F_x} \right)} \right)^2 + \frac{M_{ax}}{M_x \times \left(1 - \frac{P_{ax}}{F_x} \right)} \le 1 \right|$$





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The data contained in this literature was current as of the date of publication. Updates and changes may be made based on later testing. If verification is needed that the data is still current, please contact the Hilti Technical Support Specialists at 1-800-879-8000 (U.S.) or 1-800-363-4458 (Canada). All published load values contained in this literature represent the result of testing by Hilti or test organizations. Local base materials were used. Because of variations in materials, on-site testing is necessary to determinate performance at any specific site.